

1. Want to derive

$$\rho \frac{d\vec{v}}{dt} = -\nabla P + \frac{1}{c} (\vec{j} \times \vec{B}) \quad (13.3 \text{ G\&L})$$

from $\rho_j [(\vec{v}_j \cdot \nabla) \vec{v}_j + \frac{\partial \vec{v}_j}{\partial t}] = \rho_j^c \vec{E} + \rho_j^c (\vec{v}_j \times \vec{B}) - \nabla P_j \quad (6.25)$

\uparrow mass density \uparrow charge density $\rho_j^c = n_j q_j$

① $(\vec{v}_j \cdot \nabla) \vec{v}_j + \frac{\partial \vec{v}_j}{\partial t} = \frac{d\vec{v}_j}{dt}$

② for ions and electrons, (6.25) becomes

$$\rho_i \frac{d\vec{v}_i}{dt} = n_i q_i \vec{E} + n_i q_i (\vec{v}_i \times \vec{B}) - \nabla P_i$$

$$\rho_e \frac{d\vec{v}_e}{dt} = n_e q_e \vec{E} + n_e q_e (\vec{v}_e \times \vec{B}) - \nabla P_e$$

Add these two eqn. together, get

$$\rho_i \frac{d\vec{v}_i}{dt} + \rho_e \frac{d\vec{v}_e}{dt} = \underbrace{(n_i q_i + n_e q_e)}_0 \vec{E} + (n_i q_i \vec{v}_i + n_e q_e \vec{v}_e) \times \vec{B} - (\nabla P_i + \nabla P_e)$$

0, due to neutrality in plasma.

$$\vec{j} = n_i q_i \vec{v}_i + n_e q_e \vec{v}_e$$

$$\nabla P = \nabla P_i + \nabla P_e$$

Also, let $\rho_i \frac{d\vec{v}_i}{dt} + \rho_e \frac{d\vec{v}_e}{dt} = \rho \frac{d\vec{v}}{dt}$

$$\Rightarrow \rho \frac{d\vec{v}}{dt} = \vec{j} \times \vec{B} - \nabla P$$

This is equivalent to (13.3 G&L), $\frac{1}{c}$ is due to different unit system

2. To derive $p + \frac{B^2}{2\mu_0} = \text{constant}$.

(13.2 G&L) at steady state.

$$-\nabla p + \vec{j} \times \vec{B} = 0$$

Maxwell equation, $\nabla \times \vec{B} = \mu_0 \vec{j} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$ due to steady state.

$$\Rightarrow \nabla p = \frac{1}{\mu_0} (\nabla \times \vec{B}) \times \vec{B}$$

$$\begin{aligned} \text{With } (\nabla \times \vec{B}) \times \vec{B} &= (\vec{B} \cdot \nabla) \vec{B} - \nabla (\vec{B} \cdot \vec{B}) \\ &= -\frac{1}{2} \nabla B^2 \end{aligned}$$

$$\text{We get } \nabla p = -\frac{1}{2\mu_0} \nabla B^2$$

$$\nabla \left(p + \frac{1}{2\mu_0} B^2 \right) = 0$$

$$\begin{aligned} p + \frac{B^2}{2\mu_0} &= \text{constant} \\ &= \frac{B_0^2}{2\mu_0} \end{aligned}$$

3. Refer to Pg. 488 - Pg. 490

$$0 = -\nabla p_0 + \frac{1}{c} (\vec{j}_0 \times \vec{B}_0)$$

With linear perturbation, $p = p_0 + p'$, $\vec{j} = \vec{j}_0 + \vec{j}'$, $\vec{B} = \vec{B}_0 + \vec{B}'$

$$\text{It becomes } -\nabla p' + \frac{1}{c} (\vec{j}' \times \vec{B}_0 + \vec{j}_0 \times \vec{B}') = 0 \quad (1)$$

$$(13.5) \quad \nabla \times \vec{B} = \frac{4\pi}{c} \vec{j} \Rightarrow \begin{cases} \nabla \times \vec{B}_0 = \frac{4\pi}{c} \vec{j}_0 & (2) \\ \nabla \times \vec{B}' = \frac{4\pi}{c} \vec{j}' & (3) \end{cases}$$

$$\text{Also, } \vec{B}' = \nabla \times (\vec{\xi} \times \vec{B}_0) \quad (4)$$

$$\vec{p}' = -\gamma p_0 \nabla \cdot \vec{\xi} - \vec{\xi} \cdot \nabla p_0 \quad (5)$$

$$\Rightarrow 0 = \nabla (\gamma p_0 \nabla \cdot \vec{\xi} + \vec{\xi} \cdot \nabla p_0) + \frac{1}{4\pi} [\nabla \times \nabla \times (\vec{\xi} \times \vec{B}_0) \times \vec{B}_0 + \nabla \times \vec{B}_0 \times \nabla \times (\vec{\xi} \times \vec{B}_0)]$$

4. 13.17-13.18

$$\delta W = \int_V \left[\underbrace{\frac{Q^2}{4\pi}}_A - \underbrace{j \cdot Q \times \vec{\zeta}}_A + \gamma P_0 (\underbrace{\nabla \cdot \vec{\zeta}}_B)^2 + (\underbrace{\nabla \cdot \vec{\zeta}}_B) (\underbrace{\vec{\zeta} \cdot \nabla p}_B) \right] d^3x$$

$$- \frac{1}{2} \int_S \underbrace{(\vec{n} \cdot \vec{\zeta})}_B \left[\underbrace{\gamma P_0 \nabla \cdot \vec{\zeta}}_B + \underbrace{\vec{\zeta} \cdot \nabla P_0}_B - \frac{1}{4\pi} \underbrace{\vec{B}_0 \cdot Q}_A \right] ds$$

Here, A means "current driven" term.

B means "pressure driven" term.

$$(Q \equiv \nabla \times (\vec{\zeta} \times \vec{B}_0) = \vec{B}', \text{ is related to } \vec{j}')$$

In stellarator, B field shear is not achieved using current, so there is no "current-driving" instability. In this sense, stellarator is more stable than Tokamak.

5. (a) $b_i = \frac{B_z(\text{int})}{B_0}$ } In this case, the internal B field equals to $B_z(\text{int})$ and the external B field equals to B_0 .

$B_z(\text{ext}) = 0$

Pressure balance $P_{kin} + P_{int} = P_{ext}$

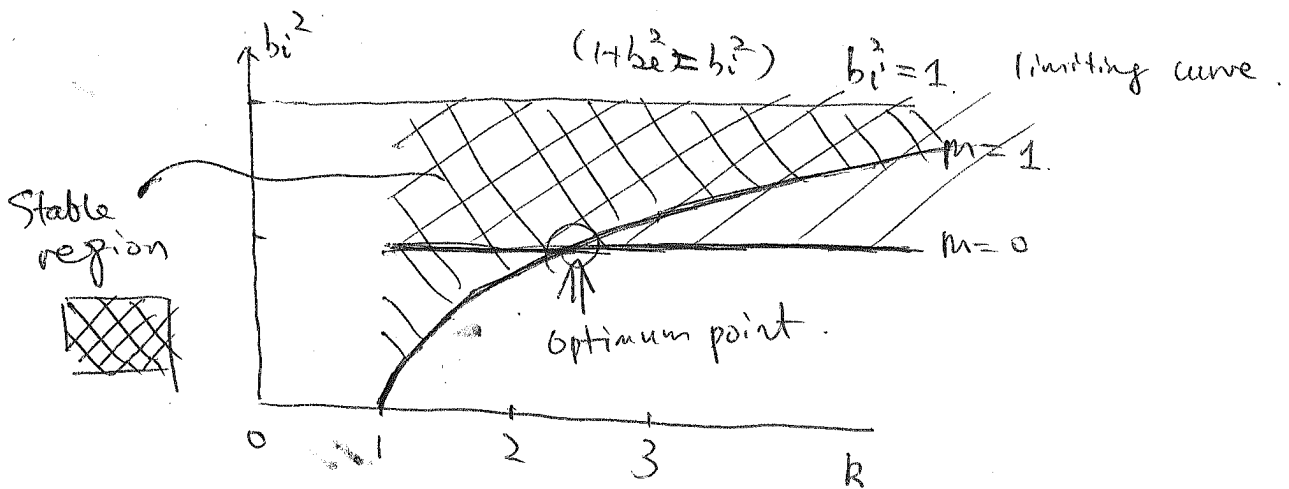
$$2nKT + \frac{B_z^2(\text{int})}{2\mu} = \frac{B_0^2}{2\mu}$$

$$\text{So, } b_i^2 = \frac{B_z^2(\text{int})}{B_0^2} = 1 - \frac{2nKT}{B_0^2/2\mu} = 1 - \beta^*$$

(b). Based on Fig. 13.2

For $\beta_2(\text{ext}) = 0$, i.e., $b_e = 0$

	$k=1$	$k=1.5$	$k=2$	$k=3$	$k=\infty$
b_i ($m=1$)	0	0.5	0.6	0.75	1
b_i^2 ($m=1$)	0	0.25	0.36	0.56	1
b_i ($m=0$)	0.7	0.7	0.7	0.7	0.7
b_i^2 ($m=0$)	0.49	0.49	0.49	0.49	0.49



Stable within the area b/w the curve and the limiting curve $b_i^2 = 1$.
($m=1$)
($m=0$)

(c) Optimum operation requires highest β and highest k .

lowest b_i^2 , $\leftarrow b_i^2 = 1 - \beta$
so $b_i^2 = 0.49$.

\rightarrow to give high power density

So, the optimum point is found as shown above.

$$\textcircled{c} \text{ A) } -\rho \Omega^2 \xi = \nabla(\gamma \rho \nabla \cdot \xi) - \frac{1}{4\pi} B \times (\nabla \times Q) \quad \text{where } \xi = [\xi_r(r) \xi_\theta(r) \xi_z(r)] \exp(im\theta + ikz)$$

From variational method and SWF: $Q_r = ikB_z \xi_r$

$$Q_\theta = ikB_z \xi_\theta$$

$$Q_z = -B_z \left[\frac{1}{r} \partial_r(r \xi_r) + \frac{im}{r} \xi_\theta \right]$$

The above equation can then be separated into:

$$-\rho \Omega^2 \xi_r = \partial_r(\gamma \rho \nabla \cdot \xi) - \frac{B_z}{4\pi} (\partial_r Q_z - ik Q_r)$$

$$-\rho \Omega^2 \xi_\theta = \frac{im}{r} (\gamma \rho \nabla \cdot \xi) - \frac{B_z}{4\pi} \left(\frac{im}{r} Q_z - ik Q_\theta \right)$$

$$-\rho \Omega^2 \xi_z = ik (\gamma \rho \nabla \cdot \xi)$$

$$\Psi = \gamma \rho \nabla \cdot \xi - \frac{1}{4\pi} B \cdot Q = (\gamma \rho + \frac{B_z^2}{4\pi}) \left[\frac{1}{r} \partial_r(r \xi_r) + \frac{m}{r} \xi_\theta \right] + ik \gamma \rho \xi_z$$

The above terms can then be rewritten with Ψ as:

$$\left(\frac{k^2 B_z^2}{4\pi} - \rho \Omega^2 \right) \xi_r = \partial_r \Psi$$

$$\left(\frac{k^2 B_z^2}{4\pi} - \rho \Omega^2 \right) \xi_\theta = \frac{m}{r} \Psi$$

$$\left[\frac{k^2 B_z^2}{4\pi} - \rho \Omega^2 \left(1 + \frac{B_z^2}{4\pi \gamma \rho} \right) \right] \xi_r = ik \Psi$$

These values can be substituted into the above equation for Ψ which results in:

$$\frac{\partial^2 \Psi}{\partial r^2} + \frac{1}{r} \frac{\partial \Psi}{\partial r} - \left(k^2 + \frac{m^2}{r^2} \right) \Psi = 0$$

$$\text{where } k^2 = \frac{\frac{k^2 B_z^2}{4\pi} - \rho \Omega^2}{\gamma \rho + \frac{B_z^2}{4\pi}} \left\{ 1 + \frac{k^2 \gamma \rho}{\frac{k^2 B_z^2}{4\pi} - \rho \Omega^2 \left(1 + \frac{B_z^2}{4\pi \gamma \rho} \right)} \right\}$$

$$b) r^2 \frac{\partial^2 \psi}{\partial r^2} + r \frac{\partial \psi}{\partial r} - k^2 r^2 \psi - m^2 \psi = 0$$

This is modified Bessel's equation

$$x^2 \frac{d^2 y}{dx^2} + x \frac{dy}{dx} - (x^2 + \alpha^2) y = 0$$

$$\psi = C_1 I_m(kr) + C_2 K_m(kr)$$

$$\textcircled{7} \quad \mu = \frac{B_0}{r B_2} \quad \frac{r}{4} \left(\frac{1}{\mu} \cdot \frac{\partial \mu}{\partial r} \right)^2 + \frac{B_0}{B_2^2} \left(\frac{\partial \mu}{\partial r} \right) > 0$$

$$\frac{\partial \mu}{\partial r} = -\frac{1}{r^2} \cdot \frac{B_0}{B_2} \quad \frac{1}{\mu} = \frac{r B_2}{B_0}$$

$$\text{Shear} = \frac{1}{\mu} \cdot \frac{\partial \mu}{\partial r} = \frac{r B_2}{B_0} \cdot -\frac{1}{r^2} \cdot \frac{B_0}{B_2} \quad \text{so Shear} = \left| -\frac{1}{r} \right|$$

At $r=0$, shear $\rightarrow \infty$

At $r=a$, shear = $\left| -\frac{1}{a} \right|$

• Shear is smaller on the outer radius which makes sense because the radius is larger so the shear is less.